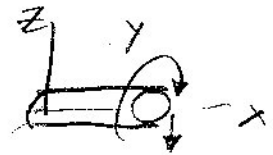


1. A circular shaft of constant diameter,  $d$ , is subject to a maximum bending moment,  $M$ , and a maximum applied torque,  $T$ . If the shaft does NOT rotate, use the Distortion Energy Theory of Failure to show that the minimum shaft diameter is given by:

$$d = \left[ \frac{16n}{\pi S_y} (4M^2 + 3T^2)^{1/2} \right]^{1/3}$$



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where,  $S_y$  is the yield strength, and  $n$  is the safety factor.

$$SF = \frac{S_y}{\sigma_e}$$

$$\sigma_x = \frac{M d}{2 I} = \frac{M d}{\frac{2\pi}{64} d^4} = \frac{32 M}{\pi d^3}$$

$$\tau_{xy} = \frac{T \frac{d}{2}}{\frac{\pi}{32} d^4} = \frac{16 T}{\pi d^3}$$

$$\sigma^1 = \sqrt{\left(\frac{32M}{\pi d^3}\right)^2 + \frac{6 \left[\left(\frac{16T}{\pi d^3}\right)^2\right]}{2}}$$

$$\frac{32^2}{\pi^2} \frac{M^2}{d^6} + \frac{3(16^2)T^2}{\pi^2 d^6}$$

$$\sigma^1 = \sqrt{\frac{1024M^2}{\pi^2 d^6} + \frac{768 T^2}{\pi^2 d^6}}$$

$$n = \frac{S_y}{\sigma^1}$$

$$\frac{16}{\pi d^3} \sqrt{4M^2 + 3T^2}$$

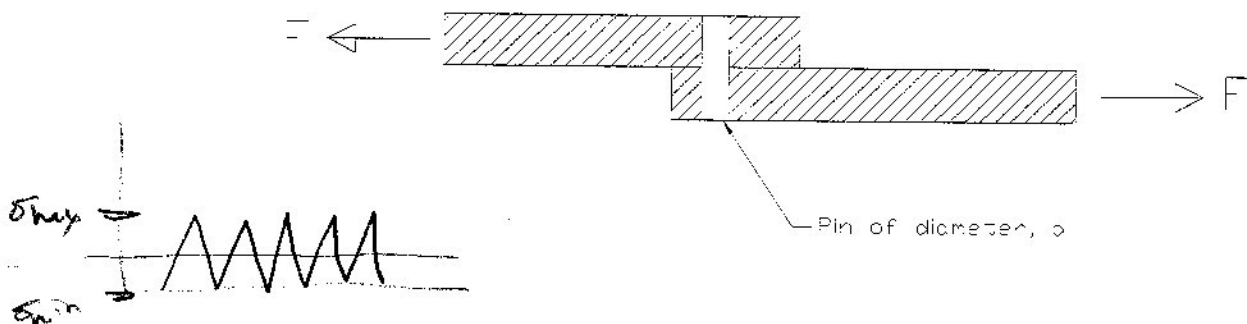
$$\Rightarrow n = \frac{\pi d^3 S_y}{16 \sqrt{4M^2 + 3T^2}}$$

$$d^3 = \frac{16n}{S_y \pi} \sqrt{4M^2 + 3T^2} \Rightarrow d = \left[ \frac{16n}{S_y \pi} \sqrt{4M^2 + 3T^2} \right]^{1/3}$$

2. The lap joint shown below is held together by a single, circular, steel pin of diameter,  $d$ , and subject to a repeated load,  $F$ .

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2 Plates, Lap Jointed



If the corrected endurance limit of the pin is known to be 35% of the ultimate tensile strength, derive an expression for the minimum pin diameter required for a safe design by using the appropriate failure theory. (Your answer should be in terms of safety factor, SF; repeated load, F; and ultimate tensile strength,  $S_{ut}$ .)

$S_n = 0.35 S_{ut}$  ✓  $d(SF, F, S_{ut})$

$\sigma_m = \sigma_a$  ✓  $\sigma_{max} = \frac{F}{\pi d^2} = \frac{4F}{\pi d^2}$   $\frac{2F}{\pi d^2} = T_m = T_a$  ✓  $\sigma_{a,1} = \sigma_{m,1} = \frac{2F}{\pi d^2}$   $\sigma_{m,3} = -\frac{2F}{\pi d^2} = \sigma_{a,3}$  +16

Safety Factor Eqn's.

$\frac{\sigma_a'}{S_n} + \frac{\sigma_m'}{S_u} = \frac{1}{SF}$  (Infinite Life)  $\frac{1}{SF} = \frac{\sigma'_{max}}{S_y}$  ✓

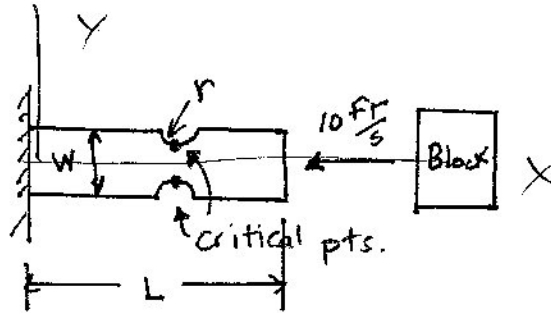
Since the answer must have a  $S_{ut}$  term I will not solve using the static failure theory but the infinite life theory. ✓

$\sigma_m' = \sqrt{\left(\frac{2F}{\pi d^2}\right)^2 + \left(-\frac{2F}{\pi d^2}\right)^2 + \left(\frac{2F}{\pi d^2}\right)^2} = \sqrt{3} \frac{2F}{\pi d^2} = \sigma_m' = \sigma_a'$  +16

$\frac{\frac{2\sqrt{3} F}{\pi d^2}}{0.35 S_{ut}} + \frac{\frac{2\sqrt{3} F}{\pi d^2}}{S_{ut}} = \frac{1}{SF} \Rightarrow \left( \frac{2\sqrt{3} F}{0.35 \pi d^2 S_{ut}} + \frac{2\sqrt{3} F}{\pi d^2 S_{ut}} = \frac{1}{SF} \right)^{-1}$  ✓

# Stupid mistake! In Compression!!

3. A notched rectangular bar is constructed of ASTM 40 Gray Cast Iron. The bar is subjected to an impact loading from block that weighs 5 lbs and is traveling at 10 ft/sec. The radius of the semi-circular notch is  $r=0.10''$ , the width of the bar is  $w=1.0''$  and its thickness into the page is,  $t=0.5''$ .



$S_{UT} = 42.5 \text{ ksi}$

a) 10  
b) 16

$W = 5$   
 $V_b = 10 \frac{\text{ft}}{\text{s}}$

$r = .1''$

$L = 10''$

$w = 1'' \quad t = .5'' \quad L = 10''$

Find:

- What failure theory would you use to evaluate failure?
- Using the failure theory from part a., compute the safety factor for the critical point on the surface of the bar. Does it fail?

Modified Mohr

$H = 1 \quad r = .1 \quad \frac{r}{h} = \frac{1}{8} \quad \frac{H}{h} = \frac{1}{.8}$   
 $h = .8 \quad .125 \quad 1.25$

$\sigma = K_t \frac{P}{A}$

From chart  $K_t = 2.3$

Now we need equivalent force of block when impacts  
 $E = 15e6 \text{ psi}$  selected min from table

$F_e = A \sqrt{\frac{2UE}{AL}} = .5 \sqrt{\frac{2 \cdot 5 \cdot 15e6}{.5(10)}} = .5 \sqrt{\frac{32.2}{12} (120)^2 15e6}$

$F_e = 11821.656 \text{ lb}$

$\sigma_x = \frac{2.3 (11821.656 \text{ lb})}{.8'' (.5)''} = 67.9745 \text{ ksi} \quad \text{--- compression}$

Since no applied torque

$\sigma_1 = \sigma_x$   
 $\sigma_2 = 0$   
 $\sigma_3 = 0$