

**3-119E** A piston-cylinder device that is filled with water is cooled. The final pressure and volume of the water are to be determined.

*Analysis* The initial specific volume is

$$v_1 = \frac{V_1}{m} = \frac{2.649 \text{ ft}^3}{1 \text{ lbm}} = 2.649 \text{ ft}^3/\text{lbm}$$

This is a constant-pressure process. The initial state is determined to be superheated vapor and thus the pressure is determined to be

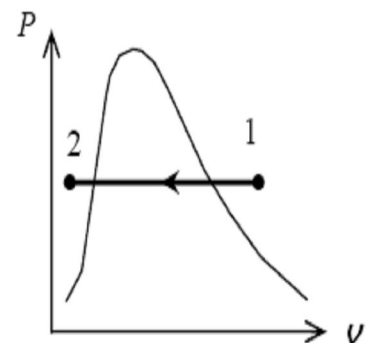
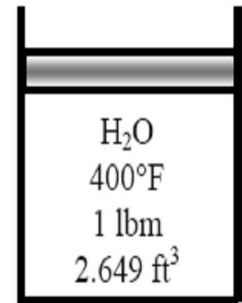
$$\left. \begin{array}{l} T_1 = 400^\circ\text{F} \\ v_1 = 2.649 \text{ ft}^3/\text{lbm} \end{array} \right\} P_1 = P_2 = \mathbf{180 \text{ psia}} \text{ (Table A - 6E)}$$

The saturation temperature at 180 psia is 373.1°F. Since the final temperature is less than this temperature, the final state is compressed liquid. Using the incompressible liquid approximation,

$$v_2 = v_f @ 180^\circ\text{F} = 0.01613 \text{ ft}^3/\text{lbm} \text{ (Table A - 4E)}$$

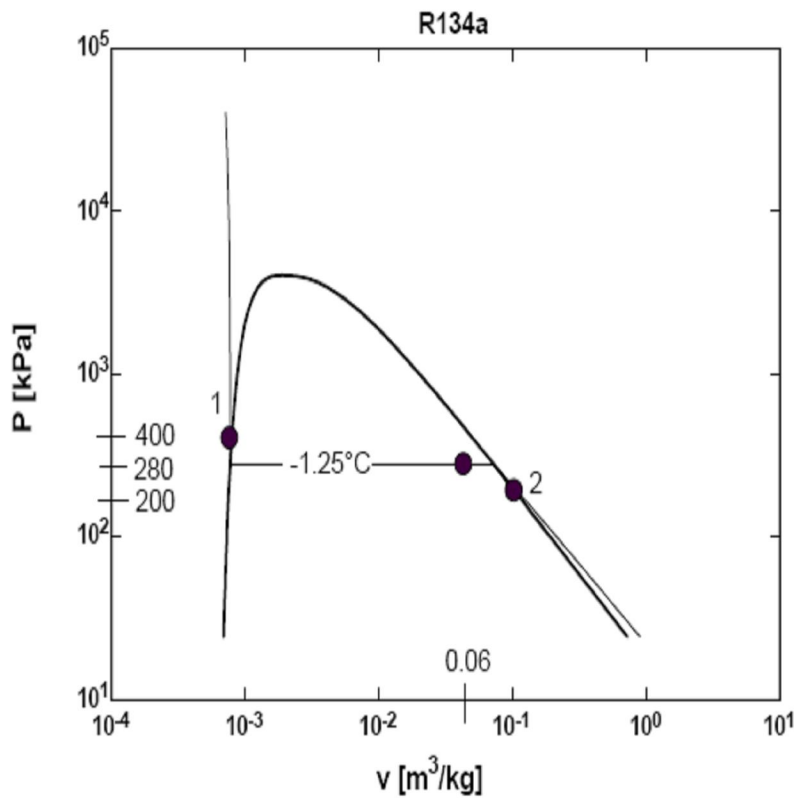
The final volume is then

$$V_2 = m v_2 = (1 \text{ lbm})(0.01613 \text{ ft}^3/\text{lbm}) = \mathbf{0.01613 \text{ ft}^3}$$

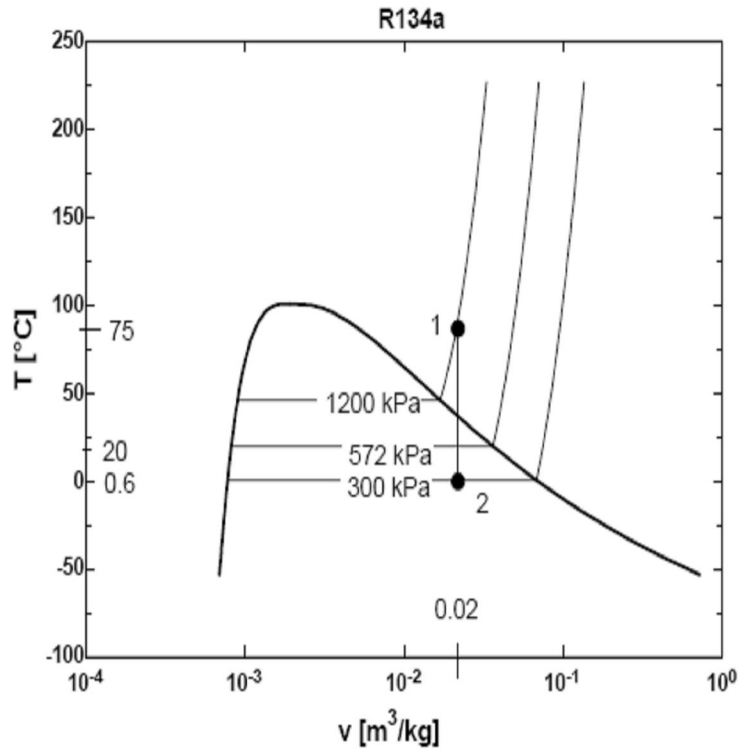


3-141

(a) On the  $P$ - $\nu$  diagram the constant temperature process through the state  $P = 280$  kPa,  $\nu = 0.06$  m<sup>3</sup>/kg as pressure changes from  $P_1 = 400$  kPa to  $P_2 = 200$  kPa is to be sketched. The value of the temperature on the process curve on the  $P$ - $\nu$  diagram is to be placed.



(b) On the  $T$ - $v$  diagram the constant specific volume process through the state  $T = 20^\circ\text{C}$ ,  $v = 0.02 \text{ m}^3/\text{kg}$  from  $P_1 = 1200 \text{ kPa}$  to  $P_2 = 300 \text{ kPa}$  is to be sketched. For this data set the temperature values at states 1 and 2 on its axis is to be placed. The value of the specific volume on its axis is also to be placed.



**4-39** A cylinder is initially filled with saturated liquid water at a specified pressure. The water is heated electrically as it is stirred by a paddle-wheel at constant pressure. The voltage of the current source is to be determined, and the process is to be shown on a  $P$ - $\nu$  diagram.

**Assumptions** 1 The cylinder is stationary and thus the kinetic and potential energy changes are zero. 2 The cylinder is well-insulated and thus heat transfer is negligible. 3 The thermal energy stored in the cylinder itself is negligible. 4 The compression or expansion process is quasi-equilibrium.

**Analysis** We take the contents of the cylinder as the system. This is a closed system since no mass enters or leaves. The energy balance for this stationary closed system can be expressed as

$$\underbrace{E_{\text{in}} - E_{\text{out}}}_{\substack{\text{Net energy transfer} \\ \text{by heat, work, and mass}}} = \underbrace{\Delta E_{\text{system}}}_{\substack{\text{Change in internal, kinetic,} \\ \text{potential, etc. energies}}}$$

$$W_{e,\text{in}} + W_{\text{pw},\text{in}} - W_{b,\text{out}} = \Delta U \quad (\text{since } Q = \text{KE} = \text{PE} = 0)$$

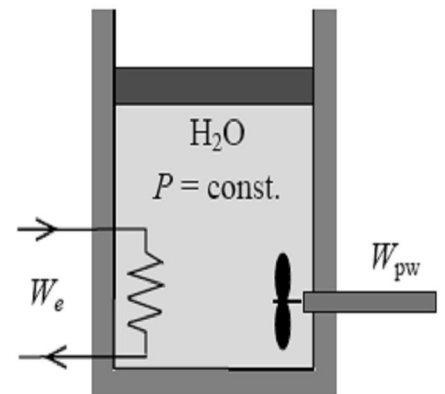
$$W_{e,\text{in}} + W_{\text{pw},\text{in}} = m(h_2 - h_1)$$

$$(\mathbf{VI}\Delta t) + W_{\text{pw},\text{in}} = m(h_2 - h_1)$$

since  $\Delta U + W_b = \Delta H$  during a constant pressure quasi-equilibrium process. The properties of water are (Tables A-4 through A-6)

$$\left. \begin{array}{l} P_1 = 175 \text{ kPa} \\ \text{sat.liquid} \end{array} \right\} \begin{array}{l} h_1 = h_f @ 175 \text{ kPa} = 487.01 \text{ kJ/kg} \\ \nu_1 = \nu_f @ 175 \text{ kPa} = 0.001057 \text{ m}^3/\text{kg} \end{array}$$

$$\left. \begin{array}{l} P_2 = 175 \text{ kPa} \\ x_2 = 0.5 \end{array} \right\} h_2 = h_f + x_2 h_{fg} = 487.01 + (0.5 \times 2213.1) = 1593.6 \text{ kJ/kg}$$



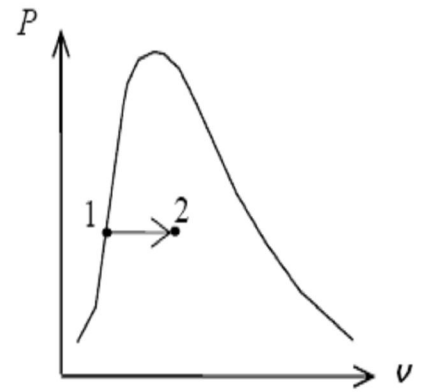
$$m = \frac{V_1}{\nu_1} = \frac{0.005 \text{ m}^3}{0.001057 \text{ m}^3/\text{kg}} = 4.731 \text{ kg}$$

Substituting,

$$VI\Delta t + (400\text{kJ}) = (4.731 \text{ kg})(1593.6 - 487.01)\text{kJ/kg}$$

$$VI\Delta t = 4835 \text{ kJ}$$

$$V = \frac{4835 \text{ kJ}}{(8 \text{ A})(45 \times 60 \text{ s})} \left( \frac{1000 \text{ VA}}{1 \text{ kJ/s}} \right) = \mathbf{223.9 \text{ V}}$$



**4-57** A spring-loaded piston-cylinder device is filled with nitrogen. Nitrogen is now heated until its volume increases by 10%. The changes in the internal energy and enthalpy of the nitrogen are to be determined.

**Properties** The gas constant of nitrogen is  $R = 0.2968 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K}$ . The specific heats of nitrogen at room temperature are  $c_v = 0.743 \text{ kJ/kg}\cdot\text{K}$  and  $c_p = 1.039 \text{ kJ/kg}\cdot\text{K}$  (Table A-2a).

**Analysis** The initial volume of nitrogen is

$$V_1 = \frac{mRT_1}{P_1} = \frac{(0.010 \text{ kg})(0.2968 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K})(27 + 273 \text{ K})}{120 \text{ kPa}} = 0.00742 \text{ m}^3$$

The process experienced by this system is a linear  $P$ - $v$  process. The equation for this line is

$$P - P_1 = c(V - V_1)$$

where  $P_1$  is the system pressure when its specific volume is  $v_1$ . The spring equation may be written as

$$P - P_1 = \frac{F_s - F_{s,1}}{A} = k \frac{x - x_1}{A} = \frac{kA}{A^2}(x - x_1) = \frac{k}{A^2}(V - V_1)$$

Constant  $c$  is hence

$$c = \frac{k}{A^2} = \frac{4^2 k}{\pi^2 D^4} = \frac{(16)(1 \text{ kN/m})}{\pi^2 (0.1 \text{ m})^4} = 16,211 \text{ kN/m}^5$$

The final pressure is then

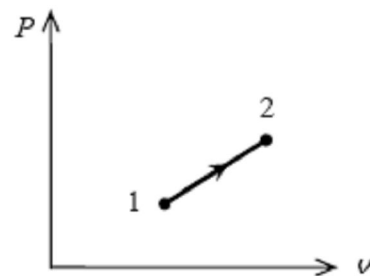
$$\begin{aligned} P_2 &= P_1 + c(V_2 - V_1) = P_1 + c(1.1V_1 - V_1) = P_1 + 0.1cV_1 \\ &= 120 \text{ kPa} + 0.1(16,211 \text{ kN/m}^5)(0.00742 \text{ m}^3) \\ &= 132.0 \text{ kPa} \end{aligned}$$

The final temperature is

$$T_2 = \frac{P_2 V_2}{mR} = \frac{(132.0 \text{ kPa})(1.1 \times 0.00742 \text{ m}^3)}{(0.010 \text{ kg})(0.2968 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K})} = 363 \text{ K}$$

Using the specific heats,

$$\begin{aligned} \Delta u &= c_v \Delta T = (0.743 \text{ kJ/kg}\cdot\text{K})(363 - 300)\text{K} = \mathbf{46.8 \text{ kJ/kg}} \\ \Delta h &= c_p \Delta T = (1.039 \text{ kJ/kg}\cdot\text{K})(363 - 300)\text{K} = \mathbf{65.5 \text{ kJ/kg}} \end{aligned}$$



**4-71** Oxygen is heated to experience a specified temperature change. The heat transfer is to be determined for two cases.

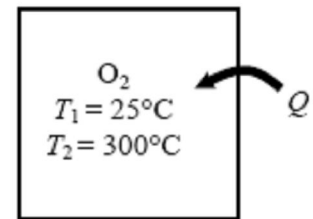
**Assumptions** 1 Oxygen is an ideal gas since it is at a high temperature and low pressure relative to its critical point values of 154.8 K and 5.08 MPa. 2 The kinetic and potential energy changes are negligible,  $\Delta ke \cong \Delta pe \cong 0$ . 3 Constant specific heats can be used for oxygen.

**Properties** The specific heats of oxygen at the average temperature of  $(25+300)/2=162.5^\circ\text{C}=436\text{ K}$  are  $c_p = 0.952\text{ kJ/kg}\cdot\text{K}$  and  $c_v = 0.692\text{ kJ/kg}\cdot\text{K}$  (Table A-2b).

**Analysis** We take the oxygen as the system. This is a *closed system* since no mass crosses the boundaries of the system. The energy balance for a constant-volume process can be expressed as

$$\underbrace{E_{\text{in}} - E_{\text{out}}}_{\text{Net energy transfer by heat, work, and mass}} = \underbrace{\Delta E_{\text{system}}}_{\text{Change in internal, kinetic, potential, etc. energies}}$$

$$Q_{\text{in}} = \Delta U = mc_v(T_2 - T_1)$$



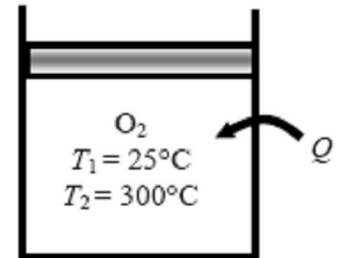
The energy balance during a constant-pressure process (such as in a piston-cylinder device) can be expressed as

$$\underbrace{E_{\text{in}} - E_{\text{out}}}_{\text{Net energy transfer by heat, work, and mass}} = \underbrace{\Delta E_{\text{system}}}_{\text{Change in internal, kinetic, potential, etc. energies}}$$

$$Q_{\text{in}} - W_{b,\text{out}} = \Delta U$$

$$Q_{\text{in}} = W_{b,\text{out}} + \Delta U$$

$$Q_{\text{in}} = \Delta H = mc_p(T_2 - T_1)$$



since  $\Delta U + W_b = \Delta H$  during a constant pressure quasi-equilibrium process. Substituting for both cases,

$$Q_{\text{in},v=\text{const}} = mc_v(T_2 - T_1) = (1\text{ kg})(0.692\text{ kJ/kg}\cdot\text{K})(300 - 25)\text{K} = \mathbf{190.3\text{ kJ}}$$

$$Q_{\text{in},p=\text{const}} = mc_p(T_2 - T_1) = (1\text{ kg})(0.952\text{ kJ/kg}\cdot\text{K})(300 - 25)\text{K} = \mathbf{261.8\text{ kJ}}$$

**4-95E** Large brass plates are heated in an oven at a rate of 300/min. The rate of heat transfer to the plates in the oven is to be determined.

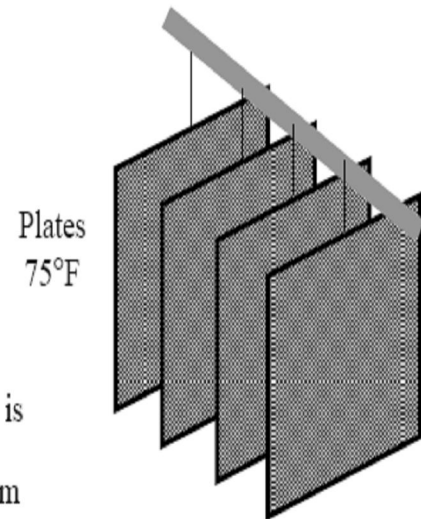
**Assumptions** 1 The thermal properties of the plates are constant. 2 The changes in kinetic and potential energies are negligible.

**Properties** The density and specific heat of the brass are given to be  $\rho = 532.5 \text{ lbm/ft}^3$  and  $c_p = 0.091 \text{ Btu/lbm}\cdot^\circ\text{F}$ .

**Analysis** We take the plate to be the system. The energy balance for this closed system can be expressed as

$$\underbrace{E_{\text{in}} - E_{\text{out}}}_{\text{Net energy transfer by heat, work, and mass}} = \underbrace{\Delta E_{\text{system}}}_{\text{Change in internal, kinetic, potential, etc. energies}}$$

$$Q_{\text{in}} = \Delta U_{\text{plate}} = m(u_2 - u_1) = mc(T_2 - T_1)$$



The mass of each plate and the amount of heat transfer to each plate is

$$m = \rho V = \rho LA = (532.5 \text{ lbm/ft}^3)[(1.2/12 \text{ ft})(2 \text{ ft})(2 \text{ ft})] = 213 \text{ lbm}$$

$$Q_{\text{in}} = mc(T_2 - T_1) = (213 \text{ lbm/plate})(0.091 \text{ Btu/lbm}\cdot^\circ\text{F})(1000 - 75)^\circ\text{F} = 17,930 \text{ Btu/plate}$$

Then the total rate of heat transfer to the plates becomes

$$\dot{Q}_{\text{total}} = \dot{n}_{\text{plate}} Q_{\text{in, per plate}} = (300 \text{ plates/min}) \times (17,930 \text{ Btu/plate}) = 5,379,000 \text{ Btu/min} = 89,650 \text{ Btu/s}$$