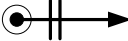
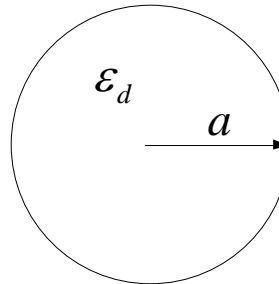


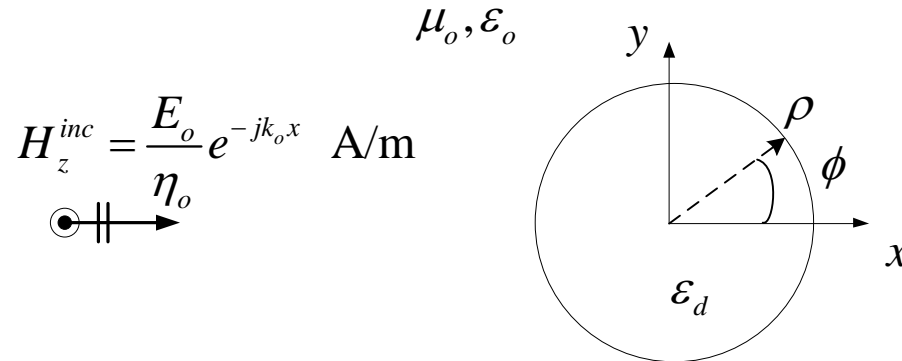
TE_z-Scattering by a Circular Dielectric Cylinder – Analytical Solution μ_o, ϵ_o

$$H_z^{inc} = \frac{E_o}{\eta} e^{-jk_o x} \text{ A/m}$$




- Consider a uniform plane wave traveling in the positive x -direction that is incident on a dielectric cylinder of radius a situated in a homogeneous free space.
- Objective:
 - Compute the total fields within the circular dielectric cylinder
 - Compute the total fields outside of the circular dielectric cylinder
- Analytical Solution
 - Based on an addition theorem expansion of the incident field into cylindrical harmonics
 - Posing the scattered field exterior to the cylinder as a superposition of cylindrical harmonics
 - Posing the total field inside to be a superposition of cylindrical harmonics
 - Enforce the boundary conditions on the surface of the cylinder

Cylindrical Harmonic Expansion of the Interior/Exterior Fields



- The incident field:

$$\circ H_z^{inc} = H_o \sum_{n=0}^{+\infty} j^{-n} \kappa_n J_n(k_o \rho) \cos(n\phi), \quad \kappa_n = 1(n=0), = 2(n \neq 0)$$

$$\circ E_\rho^{inc} = \frac{1}{j\omega\epsilon_o} \frac{1}{\rho} \frac{\partial H_z^{inc}}{\partial \phi} = -\frac{\eta_o H_o}{jk_o} \frac{1}{\rho} \sum_{n=0}^{+\infty} j^{-n} n \kappa_n J_n(k_o \rho) \sin(n\phi)$$

$$\circ E_\phi^{inc} = \frac{-1}{j\omega\epsilon_o} \frac{\partial H_z^{inc}}{\partial \rho} = j\eta_o H_o \sum_{n=0}^{+\infty} j^{-n} \kappa_n J_n'(k_o \rho) \cos(n\phi)$$

- Procedure:

- Pose H_z^{scat} ($\rho > a$) and H_z^{tot} ($\rho < a$) as cylindrical harmonic expansion
- Compute \vec{E}^{scat} ($\rho > a$) and \vec{E}^{tot} ($\rho < a$) using Maxwell's equations
- Solve for unknown coefficients by enforcing boundary conditions and orthogonality of the harmonics.

Cylindrical Harmonic Expansion of the Scat/Tot Fields

- Scattered field ($\rho > a$):

- $H_z^{scat} = H_o \sum_{n=0}^{+\infty} a_n j^{-n} \kappa_n H_n^{(2)}(k_o \rho) \cos(n\phi), \rho > a$

- $E_\phi^{scat} = j\eta_o H_o \sum_{n=0}^{+\infty} a_n j^{-n} \kappa_n H_n^{(2)'}(k_o \rho) \cos(n\phi)$

- Total field ($\rho < a$):

- $H_z^{tot} = H_o \sum_{n=0}^{+\infty} b_n j^{-n} \kappa_n J_n(k_d \rho) \cos(n\phi), \rho < a$

- $E_\phi^{tot} = j\eta_d H_o \sum_{n=0}^{+\infty} b_n j^{-n} \kappa_n J_n'(k_d \rho) \cos(n\phi)$

- where $k_d = \omega \sqrt{\epsilon_d \mu_o}$ and $\eta_d = \sqrt{\frac{\mu_o}{\epsilon_d}}$

- a_n and b_n are unknowns.

- How do we solve for them?

Solving for the Unknown Coefficients

- Boundary conditions:

- $H_z^{inc}(\rho = a^+) + H_z^{scat}(\rho = a^+) = H_z^{tot}(\rho = a^-)$

- $E_\phi^{inc}(\rho = a^+) + E_\phi^{scat}(\rho = a^+) = E_\phi^{tot}(\rho = a^-)$

- Applying orthogonality, this leads to:

$$H_o j^{-n} \kappa_n J_n(k_o a) \cos(n\phi) + H_o a_n j^{-n} \kappa_n H_n^{(2)}(k_o a) \cos(n\phi) = H_o b_n j^{-n} \kappa_n J_n(k_d a) \cos(n\phi)$$

$$j\eta_o H_o j^{-n} \kappa_n J_n'(k_o a) \cos(n\phi) + j\eta_o H_o a_n j^{-n} \kappa_n H_n^{(2)'}(k_o a) \cos(n\phi) = j\eta_d H_o b_n j^{-n} \kappa_n J_n'(k_d a) \cos(n\phi)$$

- Canceling common terms, and re-writing as a matrix equation:

- $$\begin{bmatrix} H_n^{(2)}(k_o a) & -J_n(k_d a) \\ \eta_o H_n^{(2)}(k_o a) & -\eta_d J_n'(k_d a) \end{bmatrix} \begin{bmatrix} a_n \\ b_n \end{bmatrix} = \begin{bmatrix} -J_n(k_o a) \\ -\eta_o J_n'(k_o a) \end{bmatrix}$$

- The 2×2 can be solved for a_n and b_n :

- $$a_n = \frac{\eta_d J_n'(k_d a) J_n(k_o a) - \eta_o J_n'(k_o a) J_n(k_d a)}{\eta_o J_n(k_d a) H_n^{(2)'}(k_o a) - \eta_d J_n'(k_d a) H_n^{(2)}(k_o a)}$$

- $$b_n = \eta_o \frac{J_n(k_o a) H_n^{(2)'}(k_o a) - J_n'(k_o a) H_n^{(2)}(k_o a)}{\eta_o J_n(k_d a) H_n^{(2)'}(k_o a) - \eta_d J_n'(k_d a) H_n^{(2)}(k_o a)}$$

Computing the Near-Field

- The total magnetic field H_z^{tot} can be written as:

$$\circ H_z^{tot} = \begin{cases} H_o \sum_{n=0}^{+\infty} b_n j^{-n} \kappa_n J_n(k_d \rho) \cos(n\phi), & \rho \leq a \\ H_o \sum_{n=0}^{+\infty} j^{-n} \kappa_n \left[J_n(k_o \rho) + a_n H_n^{(2)}(k_o \rho) \right] \cos(n\phi), & \rho \geq a \end{cases}$$

- To validate the MoM solution inside the cylinder, \vec{E}^{tot} is needed

$$\circ E_\rho^{tot}(\rho, \phi) = \frac{1}{j\omega\epsilon_d} \frac{1}{\rho} \frac{\partial H_z^{tot}}{\partial \phi} = -\frac{\eta_d H_o}{jk_d} \frac{1}{\rho} \sum_{n=0}^{+\infty} j^{-n} n b_n \kappa_n J_n(k_d \rho) \sin(n\phi)$$

$$\circ E_\phi^{inc} = \frac{-1}{j\omega\epsilon_d} \frac{\partial H_z^{inc}}{\partial \rho} = j\eta_d H_o \sum_{n=0}^{+\infty} j^{-n} b_n \kappa_n J_n'(k_d \rho) \cos(n\phi)$$

- Using Cartesian projections:

$$\circ E_x^{tot}(\rho, \phi) = \cos\phi E_\rho^{tot}(\rho, \phi) - \sin\phi E_\phi^{tot}(\rho, \phi)$$

$$\circ E_y^{tot}(\rho, \phi) = \sin\phi E_\rho^{tot}(\rho, \phi) + \cos\phi E_\phi^{tot}(\rho, \phi)$$

Computing the Far Field

- Often it is desirable to compute the “far” scattered field.
 - Region where the distance from the cylinder $(\rho - a) / \lambda \gg 1$
 - Also quantified as the region where $k_o \rho \gg 1$

- Asymptotic approximation of the Hankel function:

$$\lim_{k_o \rho \rightarrow \infty} H_n^{(2)}(k_o \rho) \approx \sqrt{\frac{2j}{\pi k_o \rho}} j^n e^{-jk_o \rho}$$

- Therefore, in the far field:

$$\begin{aligned} \lim_{k_o \rho \rightarrow \infty} H_z^{scat}(\rho, \phi) &= \lim_{k_o \rho \rightarrow \infty} H_o \sum_{n=0}^{+\infty} j^n (-1)^n \kappa_n a_n H_n^{(2)}(k_o \rho) \cos(n\phi) \\ &\approx H_o \sqrt{\frac{2j}{\pi k_o \rho}} e^{-jk_o \rho} \sum_{n=0}^{+\infty} j^{2n} (-1)^n \kappa_n a_n \cos(n\phi) \end{aligned}$$

- Therefore,

$$\lim_{k_o \rho \rightarrow \infty} H_z^{scat-ff}(\rho, \phi) = H_o \sqrt{\frac{2j}{\pi k_o \rho}} e^{-jk_o \rho} \sum_{n=0}^{+\infty} \kappa_n a_n \cos(n\phi)$$

Echo Width

- The echo width is the equivalent area proportional to the apparent size of the target that scatters the field in a given direction relative to the power incident from another direction.

$$\circ \sigma_{2D}(\phi) = \lim_{\rho \rightarrow \infty} (2\pi\rho\Delta z) \frac{\text{Scattered Power Density}}{\text{Incident Power Density}} = \lim_{\rho \rightarrow \infty} 2\pi\rho \frac{|H_z^{scat}|^2 \eta_o}{|H_z^{inc}|^2 \eta_o}$$

- In the far field:

$$\circ |H_z^{scat-ff}(\rho, \phi)|^2 = H_o^2 \frac{2}{\pi k_o \rho} \left| \sum_{n=0}^{+\infty} \kappa_n a_n \cos(n\phi) \right|^2$$

- Therefore

$$\circ \sigma_{2D}(\phi) = \lim_{\rho \rightarrow \infty} 2\pi\rho \frac{H_o^2 \frac{2}{\pi k_o \rho} \left| \sum_{n=0}^{+\infty} \kappa_n a_n \cos(n\phi) \right|^2 \eta_o}{H_o^2 \eta_o}$$

- or

$$\circ \sigma_{2D}(\phi) = \frac{4}{k_o} \left| \sum_{n=0}^{+\infty} \kappa_n a_n \cos(n\phi) \right|^2$$

MathCad Example

$$ka = 4 \quad \eta = 376.73031346177066 \quad \epsilon_r = 1.2 \quad \eta_d := \frac{\eta}{\sqrt{\epsilon_r}}$$

$$a_n(n) := \frac{\eta_d \cdot J_{np}(n, kda) \cdot J_n(n, ka) - \eta \cdot J_{np}(n, ka) \cdot J_n(n, kda)}{\eta \cdot J_n(n, kda) \cdot H_{n2p}(n, ka) - \eta_d \cdot J_{np}(n, kda) \cdot H_{n2}(n, ka)}$$

$$\sigma_{2dEx}(\phi) := 10 \log \left[\frac{4}{k_0} \cdot \left[\sum_{n=0}^{N_{max}} \left(\kappa(n) \cdot a_n(n) \cdot \cos \left(n \cdot \phi \cdot \frac{\pi}{180} \right) \right) \right] \right]^2$$

