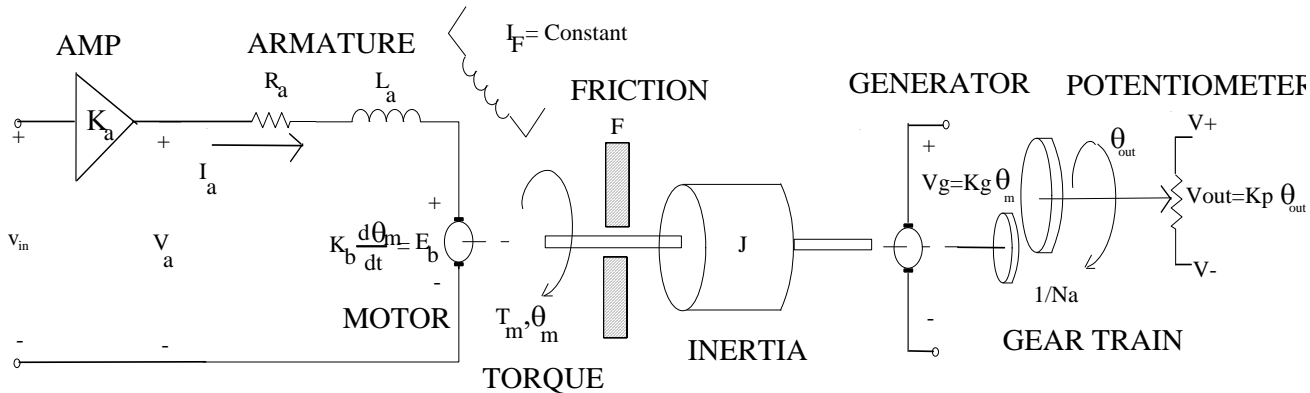


**Objective:** To study the effects of discretization and to design a feedback controller for the Motomatic DC Servo Motor

**Prelab:** (Counts as HW#10)

Due Monday, February 22

Consider the following functional block diagram for our Motomatic armature-controlled DC servomotor in our Lab:



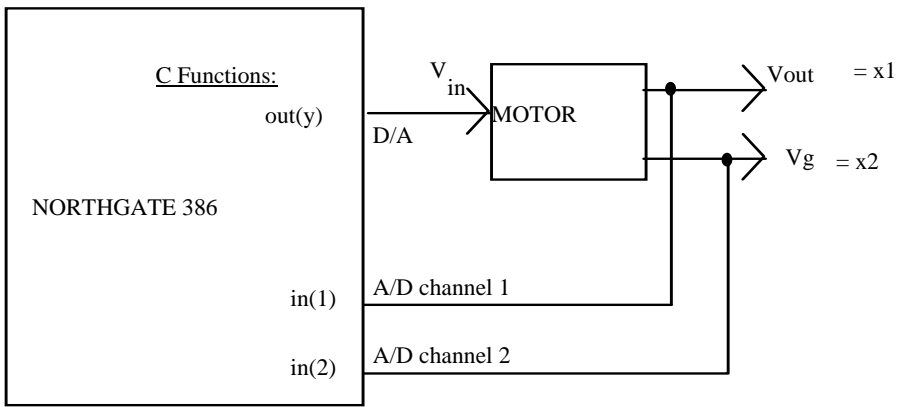
If you took EE571, you found the open-loop transfer function of the Motomatic to be:

$$\frac{V_{out}}{V_{in}} = \frac{210.9}{s^2 + 5.27s}$$

where  $V_{out}$  was the voltage off the position sensor, which was directly proportional to the shaft displacement,  $\theta_{out}$ , by the relationship  $V_{out} = K_p \theta_{out}$ . We also discovered that the voltage from the generator (tachometer),  $V_g$ , was related to the derivative of  $V_{out}$  by the following relationship:  $V_g = K_g \theta_m = K_g \frac{\theta_{out}}{N_a}$  where  $K_g$  is the generator constant and  $N_a$  is the gear ratio.

In EE571, we found the values of  $K_p = 5.139$  volts/rad,  $K_g = 0.1842$  volt/rad/sec, and  $N_a = 1/9$ , and obtained the following continuous time state variable model for the Motomatic using  $x = \begin{bmatrix} V_{out} \\ V_g \end{bmatrix}$ :  $\dot{x} = \begin{bmatrix} 0 & 3.0999 \\ 0 & -5.27 \end{bmatrix} x + \begin{bmatrix} 0 \\ 68.0346 \end{bmatrix} V_{in}$  with the output  $y = V_{out}$

- 1.a) Is the continuous model stable, marginally stable, or unstable?
  - b) Discretize the model using  $\hat{A} = e^{AT_s}$  and  $\hat{B} = \int_0^{T_s} e^{A t} B dt$  with  $T_s = 10$  msec.
  - c) Is the discrete model stable, marginally stable, or unstable? Is it controllable?
  - d) Using this discrete model, design a feedback **regulator**,  $V_{in} = -Kx_k$ , such that the Motomatic position,  $y = V_{out}$ , has no overshoot and "settles" in less than 0.3 sec. (please pick distinct eigenvalues so we can decouple the closed-loop system in part 2b)).
- 2.a) Use MATLAB's `dlsim()` function to simulate your regulator design in response to a 5 volt step (i.e., let  $V_{in} = 5 - Kx_k$ . What is the settling time? What is  $e_{ss}$  (i.e., the steady-state error,  $5 - V_{out}$ )? (Note: If you have access to SIMULINK, you may use it instead of `dlsim()`)
  - b) Recall that the settling time measures how fast the closed-loop **decoupled states** decay! Make a plot of the **decouple states** to verify the settling time (you can find the closed-loop decoupled states using the MATLAB command,  $z = \text{inv}(P) * x'$  where  $P$  is the matrix of eigenvectors of the closed-loop system,  $\hat{A} - \hat{B}K$ ).
  - c) Now design a controller so that  $V_{out}$  reaches 5 volts in steady-state while keeping the specifications of part 2a) (that is, find  $N_x$  and  $N_u$ )
  - d) Repeat parts 1d) through 2c) until all the specifications are met.
  - f) Use the `in()`, `out()`, and `sleep()` functions from Lab #1 to write a C program to implement your controller. Let us assume that we have two channels on our A/D converter and that `in(1)` will sample channel 1 where  $x_1 = V_{out}$  is connected and `in(2)` will sample channel 2 where  $x_2 = V_g$  (see below)



In the Lab: (Counts as HW#11)

Due Wednesday, February 24

1. Test your **regulator** design by choosing the regulator section of the menu, a sampling time of  $T_s=10$  msec, and an input of 5 volts. Obtain a plot and compare to Prelab results.
2. Test your **controller** design by selecting the controller option and by entering the correct values of  $N_u$  and  $N_x$ . Compare your results to the Prelab.
3. Can your closed-loop system follow a ramp? Repeat part 2 but select a 5 volt ramp input. Does your system follow a ramp?
4. How robust is your design? Repeat part 2, but start with the prony brake on the flywheel. Does your system respond well to the torque disturbance?
5. Study the effects of altering the sampling time on your system by repeating part 2 using a sampling time of 40 msec and then 80 msec (do not redesign your controller).