

EE572

Sol'n to RISHW #5*

Given the continuous state variable model, $\dot{x} = \begin{bmatrix} -1 & 0 \\ 0 & -3 \end{bmatrix}x + \begin{bmatrix} 1 \\ 2 \end{bmatrix}w$, $x(0) = \begin{bmatrix} 5 \\ 6 \end{bmatrix}$, and $y = \begin{bmatrix} 3 & 4 \end{bmatrix}x$

the corresponding discrete next-state approximation to this model,

$$x_{k+1} = \hat{A}x_k + \hat{B}w_k, \quad x_0 \text{ with sampling period } T.$$

$$y_k = \hat{C}x_k$$

- a) Calculate the zero input response for t=1,2, and 3 seconds (hint: $x_{\text{zero-input}}(t) = e^{At}x(0)$)

Sol'n: $x_{\text{zero-input}} = e^{At}x(0) = \begin{bmatrix} e^{-t} & 0 \\ 0 & e^{-3t} \end{bmatrix} \begin{bmatrix} 5 \\ 6 \end{bmatrix} = \begin{bmatrix} 5e^{-t} \\ 6e^{-3t} \end{bmatrix}$

For t=1,2, and 3 seconds: $x_{\text{zero-input}}(1) = \begin{bmatrix} 5e^{-1} \\ 6e^{-3} \end{bmatrix}$, $x_{\text{zero-input}}(2) = \begin{bmatrix} 5e^{-2} \\ 6e^{-6} \end{bmatrix}$, $x_{\text{zero-input}}(3) = \begin{bmatrix} 5e^{-3} \\ 6e^{-9} \end{bmatrix}$

- b) Find values for \hat{A} , \hat{B} , \hat{C} and x_0 if we use the approximation that $\hat{A} = I + TA$ and T=1 second and calculate the first three values of the zero-input solution for k=1,2, and 3. Compare to your answer to part a)

$$\hat{A} = I + T_s A = \begin{bmatrix} 1-1 & 0 \\ 0 & 1-3 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & -2 \end{bmatrix}, \hat{B} = T_s B = \begin{bmatrix} 2 \\ 1 \end{bmatrix} \text{ and } \hat{C} = C = \begin{bmatrix} 3 & 4 \end{bmatrix}$$

For k=1,2, and 3:

$$x_{\text{zero-input}}(1) = \hat{A}x(0) = \begin{bmatrix} 0 \\ -12 \end{bmatrix}, x_{\text{zero-input}}(2) = \hat{A}^2 x(0) = \begin{bmatrix} 0 \\ 24 \end{bmatrix}, x_{\text{zero-input}}(3) = \hat{A}^3 x(0) = \begin{bmatrix} 0 \\ -48 \end{bmatrix}$$

These are not very close to the continuous-time values!

- c) Repeat part b) using the approximation that, $\hat{A} = e^{AT}$. What conclusions can you make about the two methods of finding a discrete state model from a continuous time state model?

Sol'n:

$$\hat{A} = e^{AT_s} = \begin{bmatrix} e^{-1} & 0 \\ 0 & e^{-3} \end{bmatrix}, \hat{C} = C = \begin{bmatrix} 1 & 0 \end{bmatrix}, \text{ and}$$

$$\hat{B} = \int_0^{T_s} e^{At} dt B = A^{-1} [e^{AT_s} - I] B = \begin{bmatrix} -1 & 0 \\ 0 & -3 \end{bmatrix}^{-1} \begin{bmatrix} e^{-1} - 1 & 0 \\ 0 & e^{-3} - 1 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} = \begin{bmatrix} 2 - e^{-1} \\ -3e^{-3} + 3 \end{bmatrix}$$

For k=1,2, and 3:

$$x_{\text{zero-input}}(1) = \hat{A}x(0) = \begin{bmatrix} 5e^{-1} \\ 6e^{-3} \end{bmatrix}, x_{\text{zero-input}}(2) = \hat{A}^2 x(0) = \begin{bmatrix} 5e^{-2} \\ 6e^{-6} \end{bmatrix}, x_{\text{zero-input}}(3) = \hat{A}^3 x(0) = \begin{bmatrix} 5e^{-3} \\ 6e^{-9} \end{bmatrix}$$

These are identical to the continuous time zero-input solution evaluated at 1,2, and 3 seconds!

Conclusion: The 2nd (preferred method) of discretization preserves stability and produces a zero-input invariant model!!!

- d) For the SCALAR system, $x=aw+bw$, with output, $y=cx$, find the approximate digital transfer function, $G(z)=Y(z)/W(z)$ using:

- i) The approximation that $\hat{A} = e^{AT}$
- ii) The approximation that $\hat{A} = I + TA$
- iii) The bilinear transformation
- iv) The correct impulse invariant design method you learned in class today
- v) The correct step invariant design method you learned in class today

Solution: In continuous time, the transfer function is $H(s) = c[sI - a]^{-1}b = cb/(s-a)$. If we have a discrete model, $x_{k+1} = \hat{A}x_k + \hat{B}w_k$, is $H(z) = \hat{C}[zI - \hat{A}]^{-1}\hat{B} = \hat{c}\hat{b}/(z - \hat{a})$.

i) $H(z) = \hat{c}\hat{b}/(z - \hat{a}) = c(a^{-1}(e^{aT} - 1)b)/(z - e^{aT}) = cb(e^{aT} - 1)/a(z - e^{aT})$

ii) $H(z) = \hat{c}\hat{b}/(z - \hat{a}) = Tcb/(z - (1 + Ta))$

iii) $H(z) = H(s)|_{\frac{2(z-1)}{T(z+1)}} = cb / \left(\frac{2(z-1)}{T(z+1)} - a \right) = \frac{cb \frac{T}{2} (z+1)}{(1 - a \frac{T}{2})z - (1 + a \frac{T}{2})} = \frac{cb \frac{T}{2(1-a \frac{T}{2})} (z+1)}{z - \frac{(1+a \frac{T}{2})}{(1-a \frac{T}{2})}}$

iv) $H(s) = cb/(s-a)$. $W(s) = 1$, thus $Y(s) = cb/(s-a)$ and $y(t) = cbe^{at}u(t)$. $y(kT) = cbe^{akt}u(kT)$ and $Y(z) = cb/(z - e^{aT})$ and $W(z) = 1/T$. Thus, $H(z) = Y(z)/W(z) = cbT/(z - e^{aT})$.

v) $H(s) = cb/(s-a)$. $W(s) = 1/s$, thus $Y(s) = cb/(s(s-a))$ and $y(t) = cb/a(1 - e^{-at})u(t)$. $y(kT) = cb/a(1 - e^{-akt})u(kT)$ and $Y(z) = cb/a[z/(z-1) - z/(z - e^{aT})]$ and $W(z) = z/z-1$. Thus, $H(z) = Y(z)/W(z) = cb/a[1 - (z-1)/(z - e^{aT})] = cb/a[(1 - e^{-aT})/(z - e^{aT})]$

e) Are any of your answers for $G(z)$ the same? What if $T=1$ sec?

The step invariant and the preferred method give the same answer. This is expected since the preferred method assumes that the input is piecewise constant and a step input is definitely piecewise constant!