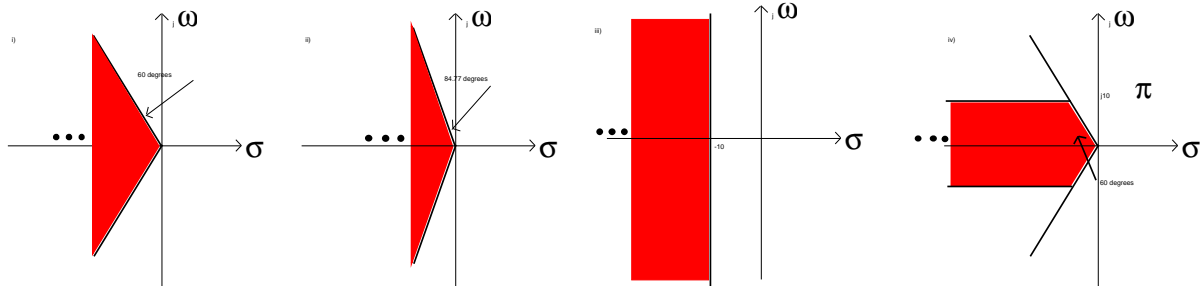


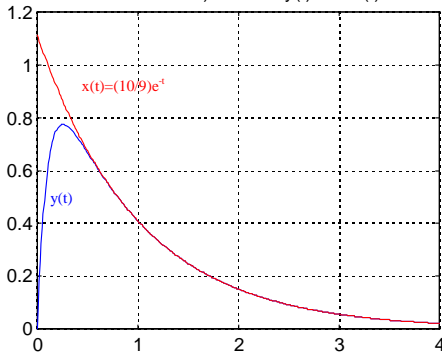
EE571 Solution to HW#21

1. a) Find regions in the complex S-plane where dominant 2nd order poles can be placed to satisfy the following transient response specifications:

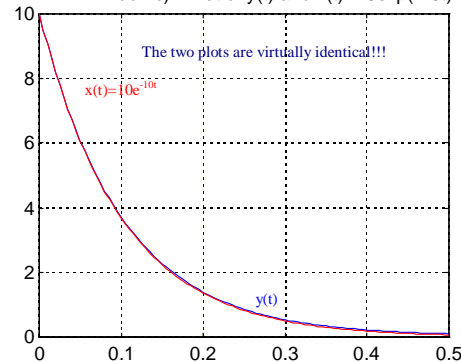


- 1b) The pole at $s=-1$ is dominant. The impulse response is $y(t)=(10/9)e^{-t} - (10/9)e^{-10t}$. See the plot below of the impulse response with the function, $x(t)=(10/9)e^{-t}$.
- c) Now, the pole at $s=-10$ is dominant because the zero at $s=-1.05$ essentially cancels the pole at $s=-1$. The impulse response is $y(t)=179/18e^{-10t} + 1/18e^{-t}$. The following is a plot of the impulse response and the function $x(t) = 10e^{-10t}$. The pole at $s=-1$ is not dominant because it is virtually cancelled out by the zero at $s=-1.05$!!!

EE571 HW#21: Prob 1b) - Plot of $y(t)$ and $x(t) = 10/9\exp(-t)$



EE571 HW#21: Prob 1c) - Plot of $y(t)$ and $x(t)=10\exp(-10t)$

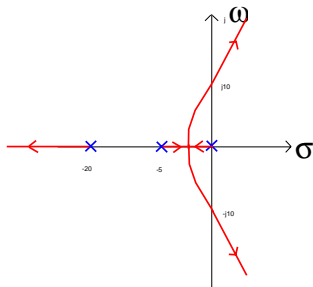


A US Navy A-6 intruder attack jet has the following open-loop transfer function for its YAW dynamics:

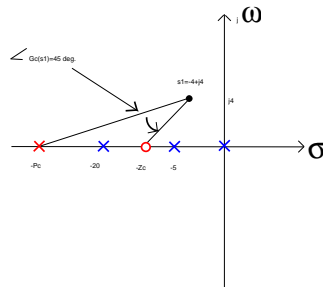
$$G(s) = \frac{30}{s(s+5)(s+20)}, \quad H(s) = 1$$

- d) The intruder transfer function is a type 1 system. Thus, $ess|_{unit\ step} = 1/(1+K_p) = 0$ and $ess|_{unit\ ramp} = 1/K_v = 100/30 = 10/3$.
- e) (See root-locus below). To determine when the closed-loop system becomes unstable, we need to construct the Routh Array for the characteristic equation, $s^3+100s^2+25s+K=0$. The closed-loop system is unstable for $0 < K < 83.33$. The root locus crosses at $s=-j10$ and $s=+j10$. Thus, the system will become unstable if we insert a gain greater than 83.33 into the forward loop.

| Routh Array | | |
|-------------|---------|-----|
| s^3 | 1 | 25 |
| s^2 | 100 | 30K |
| s^1 | 25-0.3K | |
| s^0 | 30K | |



Uncompensated Root-Locus

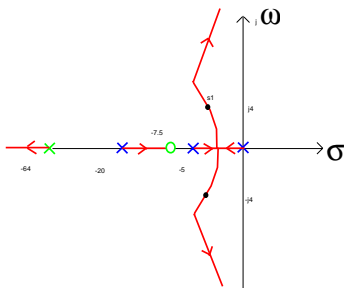


Angle of Deficiency Illustration

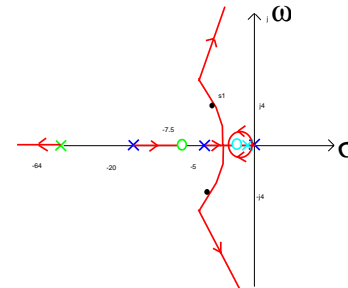
2.a) Desired dominant poles are at $s = -4 + j4$ and $s = -4 - j4$. From the root locus sketch above, it is clear that the uncompensated root locus does **not** pass thru these poles. The angle of deficiency is $\angle G_c(s_1) = 180^\circ \times \text{odd\#} - \angle G(s_1) = 180^\circ \times \text{odd\#} - \angle \frac{30}{s_1(s_1+5)(s_1+20)} = 180^\circ - 135^\circ = 45^\circ$. Therefore, our lead compensator must supply 45 degrees. The form of G_c is $G_c(s) = K_c(s+z_c)/(s+p_c)$. Let's pick z_c to be as far to the left as possible. Let z_c be 7.5 (by geometry, z_c must be less than 8). Then $\angle G_c(s_1) = 45^\circ = \angle(s_1 + 7.5) - \angle(s_1 + p_c) = 48.81^\circ - \angle(s_1 + p_c)$ or $\angle(s_1 + p_c) = 3.81^\circ$. Solving for p_c : $IM(s_1) / RE(s_1 + p_c) = \tan(3.81^\circ)$ or $p_c = IM(s_1) / \tan(3.81^\circ) - RE(s_1) = 64$. The last step is to find K_c from the magnitude condition: $K_c = 1/|G(s_1)(s_1 + z_c)/(s_1 + p_c)| = 145.07$. Thus, the lead compensator is $G_c(s) = 145.07(s+7.5)/(s+64)$.

2.b) To meet the $\text{ess|ramp} = 1/20$ spec, we need to add a **lag** compensator of the form $G_{lag} = K_{lag}(s+z_{lag})/(s+p_{lag})$ where K_{lag} is about 1 and $p_{lag} < z_{lag}$. To meet the spec, we must have $\text{ess|ramp} = 1/20 = 1/K_v$ or $K_v = 20$. Or, $20 = K_v = \lim_{s \rightarrow 0} s G_{lag} G_c G(s) = (z_{lag})(30)(145.07)(7.5) / ((p_{lag})(64)(5)(20)) = (z_{lag})(5.1) / (p_{lag})$. Thus, if we choose $p_{lag} = 0.01$, then $z_{lag} = 20p_{lag} / (5.1) = 0.0392$. Finally, we can find K_{lag} from the magnitude condition: $K_c = 1/|G_c G(s_1)(s_1 + z_{lag}) / (s_1 + p_{lag})| = 1.0037$. Thus, the lag compensator is $G_{lag}(s) = 1.0037(s+0.0392)/(s+0.01)$.

2.c) The following is a sketch of both the lead compensated and the lead-lag compensated root loci:



Lead Root Locus



Lead/Lag Root Locus

2.d) The open-loop lead compensated transfer function is $G_c G(s) = 145.07(s+7.5)(30)/(s(s+5)(s+20)(s+64))$. Thus, the closed-loop poles are the roots of $1 + G_c G = 0$ which are $-4 + j4$, $-4 - j4$, -15.6 , -65.4 (according to MATLAB's roots() function). The open-loop lead/lag compensated transfer function is $G_{lag} G_c G(s) = 1.0037(145.07)(s+0.0392)(s+7.5)(30)/(s(s+0.01)(s+5)(s+20)(s+64))$. Thus, the closed-loop poles are the roots of $1 + G_{lag} G_c G = 0$ which are -0.0394 , $-3.99 + j4.01$, $-3.99 - j4.01$, -15.6 , -65.4 (according to MATLAB's roots() function). Note, that for the closed-loop Lead/Lag system, the closed-loop pole at $s = -0.0394$ is NOT the dominant pole because it is effectively canceled by the zero of the LAG compensator located at $s = -0.0392$. Also, note that the

Lead/Lag root locus does not quite pass through the desired dominant poles at $s_1 = -4 + j4$ but passes through $-3.99 + j4.01$.