

Root Locus: Let $KGH = K \frac{s^m + bs^{m-1} + \dots}{s^n + as^{n-1} + \dots}$ be the open-loop transfer function.

Angle Condition: A point s_1 is on the R.L. if $\angle GH(s_1) = 180^\circ \times (\text{odd number})$

Magnitude Condition: If a point s_1 lies on the R.L., then the value of K can be found from $|KGH(s_1)| = 1$

- 10 rules**:
- Starts @ open loop poles @ $K=0$
 - Ends @ open loop zeroes @ $K=\infty$
 - # of branches = n
 - R.L. is symmetric WRT σ -axis and any other axis about which the open-loop pole zero configuration is symmetric
 - \angle of asymptotes = $180^\circ (\text{odd } \#)/(n-m)$
 - asymptotes are centered at $\sigma = (b-a)/(n-m)$
 - R.L. exists at a pt. on σ -axis if # of poles and zeroes of GH to the right is odd
 - To find angle of departure - draw a pt. very close to pole or zero and use \angle condition
 - Use Routh array to find pt. where R.L. crosses $j\omega$ -axis
 - Break-away and break-in pts. @ $\partial K/\partial s = 0$

Root Locus Compensation: $\angle G_c(s_1) = \text{angle of deficiency} = 180^\circ \times (\text{odd } \#) - \angle GH|_{\text{desired poles}}$; $G_{PID} = K_i/s + K_p + K_d s$

Error Analysis: (Valid for unity-feedback with closed loop system stable):

$$K_p = \lim_{s \rightarrow 0} G(s) \quad K_v = \lim_{s \rightarrow 0} sG(s) \quad K_a = \lim_{s \rightarrow 0} s^2 G(s) \quad \text{ess}|_{\text{step}} = 1/(1+K_p) \quad \text{ess}|_{\text{ramp}} = 1/K_v \quad \text{ess}|_{\text{parabola}} = 1/K_a$$

Routh Array: Check the RHP roots of $b_n s^n + b_{n-1} s^{n-1} + b_{n-2} s^{n-2} + \dots + b_1 s + b_0 = 0$

Frequency Response Methods:

Mapping Theorem: Let $F(s)$ be a ratio of two polynomials in s . Choose a closed contour and map it into the $F(s)$ - plane. Then, the number of encirclements the mapped contour makes about the origin in the $F(s)$ -plane (in the same direction as the original contour), is $N=Z-P$ where $Z = \#$ of zeroes of $F(s)$ enclosed by the original contour and $P = \#$ of poles of $F(s)$ enclosed by the original contour

s^n	b_n	b_{n-2}	$b_{n-4} \dots$
s^{n-1}	b_{n-1}	b_{n-3}	$b_{n-5} \dots$
s^{n-2}	c_1	c_2	\dots
\vdots	\vdots	$c_1 = \frac{b_{n-1}b_{n-2} - b_n b_{n-3}}{b_{n-1}}$	
s^1	\vdots	$c_2 = \frac{b_{n-1}b_{n-4} - b_n b_{n-5}}{b_{n-1}}$	
s^0	\vdots	\vdots	

Decibel: $20\log(|\cdot|)$

gain margin = $1/|GH(j\omega_{cp})|$ where $\angle GH(j\omega_{cp}) = -180^\circ$

phase margin = $180^\circ + \angle GH(j\omega_{cg})$ where $|GH(j\omega_{cg})| = 1$ or 0 dB

Conversion Factors: $2 + j = \sqrt{5} \angle 26.6^\circ$; $\sqrt{3} + j = 2 \angle 30^\circ$; $1 + j = \sqrt{2} \angle 45^\circ$; $1 + j\sqrt{3} = 2 \angle 60^\circ$; $1 + j2 = \sqrt{5} \angle 63.4^\circ$
 $1 = 0 \text{ dB}$ $2 = 6 \text{ dB}$ $3 = 9.5 \text{ dB}$ $5 = 14 \text{ dB}$ $8 = 18 \text{ dB}$

Lead Compensation

$$G_c(s) = K_c \frac{Ts+1}{\alpha Ts+1} \quad 0 < \alpha < 1$$

Maximum phase:

$$\sin \phi_m = \frac{1-\alpha}{1+\alpha} \text{ occurs at } \omega_m = 1/(\sqrt{\alpha}T)$$

$$\text{Extra gain at } \omega_m = 1/\sqrt{\alpha}$$

Lag Compensation

$$G_{lag}(s) = K_{lag} \frac{Ts+1}{\beta Ts+1} \quad 1 < \beta < \infty$$

Find $\omega_{cg\text{new}}$ such that

$$\angle GH(j\omega_{cg}) = -180^\circ + \text{desired pm} + \text{fudge factor}$$

Attenuation at high frequencies = $1/\beta$

Sensitivity: $S_y^x = \frac{\partial x}{\partial y} \frac{Y}{X} \Big|_{x_{nom}, y_{nom}}$

Observer Equation: $\dot{x} = Ax + Bw + K_o(y - Cx)$